# A two-layer model for stratocumulus clouds

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## Abstract

Mixed layer models (MLMs) have been used to improve the understanding of stratocumulus clouds. These models consider the stratocumulus-topped boundary layer as a single well-mixed slab and only require the surface and top fluxes and a source/sink term to describe the boundary layer. Stratocumulus dynamics and the influence of large-scale conditions such as the sea surface temperature on the stratocumulus cloud amount have been studied with MLMs.

Observations show that the boundary layer does not remain well-mixed when it deepens. Instead of a single mixed layer, it can be considered as two mixed layers on top of each other. This observed two-layer structure motivates to build a new model including a seperate cloud and sub-cloud layer: the two-layer model.

The two-layer model is used to study the stratocumulus to cumulus transition and is found to be capable of predicting this transition. The effect of subsidence on the liquid water path (LWP) was examined. A higher subsidence leads to a smaller LWP and a more rapid break-up of the stratocumulus clouds.

Steady-state solutions of the two-layer model showed that the change of LWP due to a warmer climate is smaller than predicted with a MLM. Where the MLM only predicts a cloud thickening, the two-layer model predicts thinning as well as thickening depending on the free tropospheric conditions.

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## 1 Introduction

Stratocumulus clouds are a shallow, low-level cloud type, typically occurring below two kilometers and with a thickness in the order of a few hundred meters. An example of a stratocumulus cloud can be seen in figure 1.1. Stratocumulus clouds are part of the atmospheric boundary layer, which is the shallow layer close to the earth where the earth surface is 'felt'. The atmospheric boundary layer is a layer of turbulent air that is separated from the lighter, laminar air above.

Shallow stratocumulus-topped boundary layers (STBLs) are often well mixed, but for deeper boundary layers the STBL begins to separate into two layers where cumulus clouds start to form underneath the stratocumulus clouds [Bretherton and Wyant, 1997].



Figure 1.1 - A sheet of stratocumulus clouds. Image from Met Office UK [2014].

Stratocumuli cover approximately one fifth of the Earth's surface in the annual mean [Wood, 2012], whereas the 80 % of the stratocumulus are located over the ocean [Warren et al., 1988]. Stratocumuli have a strong ability to cool our planet by reflecting solar radiation due to their high albedo compared to the underlying sea surface and large coverage [Dal Gesso et al., 2014b].

In climate predictions, the most uncertainties arise from the stratocumulus and stratocumulus to cumulus transition regimes [Williams and Webb, 2009]. According to Randall et al. [1984] small changes in the coverage and thickness of stratocumulus clouds lead to an offset in climate warming due to enhanced greenhouse gasses. While stratocumulus clouds now exert a cooling effect on the planet, this cooling effect may be enhanced or weakened in response to global warming, thereby producing a radiative feedback. It is therefore important to see how the stratocumulus amount changes due to climate warming.

Earlier research regarding the cloud-climate feedback has been done in several ways. The physical processes concerning low-level clouds have been studied by an intercomparison study between LES and single column models (SCMs) by Zhang et al. [2013]. They examined the steady-state response of perturbations in cloud controlling factors for three cloud regimes: well-mixed stratocumulus, decoupled stratocumulus, and cumulus.

The different LES models produce results that are consistent with each other and predict a positive cloud radiative feedback in a warmed climate for both stratocumulus and cumulus underneath stratocumulus cases, but there is a large spread in the outcomes of the SCMs both in sign and magnitude.

De Roode et al. [2012] studied the steady-state liquid water path (LWP) response of the stratocumulus-topped boundary layer to an increase in SST, using the MLM. They found that the entrainment response due to an increase in SST can be positive or negative, depending on the free tropospheric conditions. The response of the LWP can be magnified, damped or change in sign due to this entrainment response. The different parameterisations of entrainment in climate models may therefore be a plausible cause of the spread in LWP-response prediction.

Although the MLM is a suitable tool to examine well-mixed layers, it is less suitable for more complex situations such as a deepened boundary layer where stratocumulus and cumulus clouds co-exist. Observations of these cases show that the atmosphere is closer to a two-layer structure, with a warmer and dryer cloud layer as compared to the cooler and more humid sub-cloud layer below. In this research a new model is developed to describe this two-layered structure. This two-layer model is built out of two different mixed layers on top of each other. The two-layer model can be used to gain more understanding of the STBL and to study the effect of changes in large-scale conditions on the STBL.

To validate the two-layer model LES results from a stratocumulus to cumulus transition experiment are used, the Atlantic Stratocumulus Transition EXperiment (ASTEX). Because of the uncertainty in the subsidence rate during the transition [Bretherton and Pincus, 1995], a subsidence sensitivity experiment will be performed with the two-layer model. Where Bretherton and Pincus argued that decreasing the subsidence led to a more rapid break-up of the cloud layer, more recent subsidence sensitivity experiments found the opposite [Sandu and Stevens, 2011, Bretherton et al., 2013].

Besides these transient experiments, steady-state experiments are performed in addition to the experiments of de Roode et al.. The response of the LWP to a warming climate is examined, but now with a two-layer model instead of an MLM.

## 2 Thermodynamics

The presence of variable amounts of water in the atmosphere has two important effects. Firstly, it modifies the density which is the major forcing term for vertical momentum. Secondly, formation and dissipation of clouds lead to latent heat release effects, that are relevant to the heat budget of the atmosphere. In this chapter, thermodynamic laws will be used to incorporate the effects of moisture on heat and density and to obtain variables that are conserved under adiabatic processes. To indicate the amount of water dimensionless measures as the mixing ratio r or the specific humidity q can be used. The mixing ratio is a ratio of the mass of water to the total mass of water and dry air;

$$r_k = \frac{m_k}{m_d}, q_k = \frac{m_k}{m} \quad \text{where } k \in v, l, i$$

$$(2.1)$$

and with v, l and i represent the water vapor, liquid water and water in the ice phase respectively. Here  $m_d$  is the mass of dry air and the total mass of air is  $m = m_v + m_l + m_i + m_d$ . The total specific humidity is then defined by

$$q_t = q_v + q_l + q_i. (2.2)$$

#### 2.1 Potential temperature

Air parcels at different heights will experience different pressures p and temperatures T. To compare air parcels adequately, the potential temperature is introduced. The potential temperature  $\theta$  is not influenced by vertical adiabatic movement of a dry air parcel. It is defined by

$$\theta = T\left(\frac{p_0}{p}\right)^{\frac{R_d}{c_p}},\tag{2.3}$$

where  $R_d$  is the ideal gas constant for dry air,  $c_p$  the specific heat capacity at constant pressure and  $p_0$  the pressure at a reference height, which is usually taken  $p_0 = 1000$  hPa. The derivation of equation (2.3) can be found in appendix (B.1). A more convenient way of writing is

$$\theta = \frac{T}{\Pi},\tag{2.4}$$

with the exner function  $\Pi = \left(\frac{p_0}{p}\right)^{\frac{-R_d}{c_p}}$ .

#### 2.2 Liquid water potential temperature

For vertical adiabatic movement of a moist air parcel, additional effects of heating occur. If the parcel rises, at some point the specific humidity of the parcel will equal the saturation humidity. Further rising of the parcel will lead to condensation and thus in a release of latent heat. The liquid water potential temperature takes these phase changes into account and is therefore a conserved quantity for isentropic processes in cloudy atmospheres. The liquid water potential temperature is given by:

$$\theta_l = \theta - \left(\frac{L_v}{\Pi c_p}\right) q_l,\tag{2.5}$$

with  $L_v$  the specific latent heat for vaporization and  $q_l$  the liquid specific humidity [Deardorff, 1975]. The liquid temperature  $T_l$  is then again obtained from  $\theta_l$  by the exner function.

#### 2.3 Virtual potential temperature

Buoyancy is one of the driving forces for turbulence in the boundary layer. Parcels of warm air rise because they are less dense than the surrounding air, and thus positively buoyant. Virtual temperature is the temperature that dry air must have to equal the density of moist air at the same pressure and is therefore a useful variable in studies involving buoyancy. Instead of studying variations in density, variations in virtual potential temperature can be used. The virtual temperature is given by:

$$T_v = \left[1 - \left(1 - \frac{1}{\epsilon}\right)q_v - q_l\right]T,\tag{2.6}$$

with  $\epsilon = \frac{R_{\rm d}}{R_v}$ , [Stull, 1988]. The virtual potential temperature is defined as

$$\theta_v = \frac{T_v}{\Pi}.\tag{2.7}$$

### 2.4 Saturation humidity

The saturation vapor pressure at liquid temperature  $T_l$  is determined by the Tetens formula:

$$e_{s}(T_{l}) = e_{s0} \exp\left[a\frac{(T_{l} - T_{trip})}{T_{l} - b}\right],$$
with
$$e_{s0} = 610.78 \text{ Pa},$$

$$T_{trip} = 273.16 \text{ K},$$

$$a = 17.27,$$

$$b = 35.86,$$
(2.8)

[Murray, 1967]. With the saturation vapor pressure, the saturation specific humidity at temperature  $T_l$  can be calculated:

$$q_{sat} \equiv q_s(T_l, p) = \frac{R_d}{R_v} \frac{e_s(T_l)}{p - 0.378e_s(T_l)},$$
(2.9)

where  $R_v$  denotes the ideal gas constant of vapor, [Cuijpers, 1994]. To obtain the saturation humidity profile in the boundary layer, the pressure profile is needed. Using the hydrostatic pressure

$$\frac{dp}{dz} = -\rho g \tag{2.10}$$

and the gas law

$$p = \rho R_{\rm d} T_v \longrightarrow \rho = \frac{p}{R_{\rm d} T_v} \tag{2.11}$$

leads to an implicit relation for the pressure:

$$\frac{dp}{dz} = -\frac{p}{R_{\rm d}T_v}g.$$
(2.12)

#### 2.5 Liquid water path

The liquid water path (LWP) is a measure of the total amount of liquid water between two points and is calculated by

$$LWP = \int_0^h \rho_{air} q_l dz, \qquad (2.13)$$

where  $\rho_{air} = \frac{p}{R_{d}T_{v}}$  according to tthe gas law.

## 3 Physical processes of stratocumulus clouds

For the formation and maintenance of the stratocumulus, two conditions are essential. Firstly, a stable stratification in the free troposphere above the boundary layer is needed, such that deep convection is not allowed. Secondly, for the cloud formation a continuous supply of moisture is needed, which explains the frequent occurence over the oceans. A schematic overview of all the processes described in this chapter is provided in figure 3.1.



**Figure 3.1** – Schematic cross-section of a boundary layer topped with a stratocumulus cloud. The physical processes that are important in the formation and maintenance of stratocumulus clouds are indicated.

### 3.1 Radiative forcing

Radiative forcing in stratocumulus is a main driver of turbulence. The radiation considered is splitted into two wavelength bands; shortwave (SW) and longwave (LW). This is possible because the peak in the solar spectrum is at the visible light wavelengths, while the earth is emitting infrared radiation and there are no other bodies near the earth that contribute significantly to the radiation budget [Stull, 1988].

A schematic overview of the longwave radiative flux is represented in figure 3.2. The downward longwave radiative flux from the atmosphere can be described by the Boltzmann equation:

$$F_{LW,\downarrow} = \epsilon_{\rm atm} \sigma T_{\rm atm}, \qquad (3.1)$$

with  $\sigma$  the Stefan-Boltzmann constant,  $T_{\rm atm}$  the temperature of the atmosphere and  $\epsilon_{\rm atm}$  the emissivity of the atmosphere, which is smaller than 1. In general stratocumulus clouds act approximately as a black body, for a cloud thickness larger than ~ 100 m. The downward longwave radiative flux from the stratocumulus cloud can again be described by the Boltzmann equation, only with an emissivity  $\epsilon_{\rm cld}$  of approximately 1.

The emissivity of the sea surface can be approximated by  $\epsilon_{\text{sea}} \approx 0.99$  [Sidran, 1981]. The cloud and surface emissivities are approximately the same. The surface temperature is only slightly larger than the cloud temperature and therefore the cloud base is slightly warmed. Because of this small temperature difference, the upward radiative flux is hardly affected by the presence of stratocumulus and is indicated with a straight line in figure 3.2.

The jump in the downward radiative flux, as can be seen in figure 3.2, creates a cooling effect in the top of the cloud layer. The net longwave radiative flux usually has a value of around 70 W/m<sup>2</sup>, leading to a cooling rate of 5 to 10 K per hour.



**Figure 3.2** – Schematic cross-section of a boundary layer topped with a stratocumulus cloud, with an overview of the up- and downward longwave radiation.

Solar radiation also influences the cloud, but varies with time of the day, location, seasons and the presence of higher-level clouds. It is therefore harder to quantify. Incoming solar radiation is reflected, transmitted and absorbed by the stratocumulus. The relative amount of reflected solar radiation depends on the microphysical sructure of the cloud, but is typically 40 to 80 %. The amount of solar radiation absorbed by the cloud is in general less than 15 % and the rest is transmitted to the surface. The absorption of solar radiation leads to a warming of the cloud [van Zanten, 2000]. The absorption and transmission of the SW radiation is indicated

by the red arrows in figure 3.1.

### 3.2 Entrainment and subsidence

Also crucial in the development of stratocumulus clouds is entrainment: the mixing of the air above the inversion into the boundary layer. At the top of the boundary layer the rising thermals hit the inversion layer where their vertical motion is damped. Because of their momentum, however, they overshoot and after that move downwards again due to their higher density than the surrounding air. During this descent warm dry air from above the inversion is dragged along and mixed into the boundary layer; a process called entrainment [Duynkerke et al., 1999]. The entrainment rate  $w_e$  defines the rate at which the boundary layer height grows and determines the magnitude of the warming and drying of the boundary layer [van Zanten, 2000]. It is therefore an important parameter for the evolution of the cloud, but it is difficult to measure [Stevens, 2003].

A counteracting process in the growth of the boundary layer is a large-scale subsiding motion, or subsidence. This subsidence is the downward branch of the Hadley-circulation, or the downward branch of an high pressure area.

### 3.3 Turbulent mixing

Turbulent mixing is an essential process in stratocumulus-topped boundary layers. In boundary layers without stratocumulus clouds, also called clear boundary layers, the turbulence is driven by convection from the earth surface. During the day, the sun warms the ground surface and the air close to the surface. Since warm air is less dense than cold air, the warm air close to the surface will rise. Such columns of rising air are called thermals. The rising thermals will mix with the surrounding air and therefore mix heat and moisture.

For stratocumulus-topped boundary layers, the stratocumulus clouds will block the sun, thereby reducing the surface solar radiation. The main cause for the mixing here is the longwave radiative effects at the cloud top [Lilly, 1968]. The air at the cloud top is locally cooled. The cool air starts to sink and creates turbulence. This mixing creates a vertically well-mixed boundary layer, with conserved variables  $q_t$  and  $\theta_l$  that are nearly constant with height.

### 3.4 Decoupling and transition to cumulus

As air advects over warmer waters, the boundary layer deepens and decouples. The stratocumulus layer often exists within a mixed layers, called the cloud layer, but the eddies generated by the longwave cooling are not able to mix through the sub-cloud layer. The sub-cloud layer, or near-surface layer, can still be mixed by the turbulence generated by the surface as in a clear boundary layer. The sub-cloud layer is therefore also a mixed layer.

Between the vertically well-mixed sub-cloud and cloud layer a transition layer is formed. The decoupling is accompanied by the development of cumulus on top of the sub-cloud layer and thinning of the stratocumulus layer [Wyant and Bretherton, 1997].

## 4 Mixed Layer Model

The mixed layer model (MLM) is a suitable tool to understand the effect of changes in different cloud controlling factors on the cloud amount. It considers the mixed layer (ML) in which conserved variables  $\psi \in \{\theta_l, q_t\}$  are approximately constant with height because of intense vertical mixing [Stull, 1988]. In figure (4.1) a schematic representation of the mixed layer is shown, which starts at height z = 0just above the sea surface and ends at the base of the inversion layer height  $z_i$ . The vertical profiles of conserved variables in the mixed layer are indicated with  $q_{t,ML}$  and  $\theta_{l,ML}$ ,  $q_t^+$  and  $\theta_l^+$  are the values just above the inversion layer and  $\theta_{l,0}$ and  $q_{sat,0}$  are the surface values of  $q_t$  and  $\theta_l$  respectively. The cloud base height  $z_{cb}$  is determined as the level where the total specific humidity  $q_t$  is equal to the saturation specific humidity  $q_{sat}$ .

To describe the conserved variables of the mixed layer, the vertically integrated



**Figure 4.1** – Schematic representation of the mixed layer model. The mixed layer contains the cloud and sub-cloud layer. The vertical profiles of the conserved variables  $\theta_1$  and  $q_t$  are indicated. The free tropospheric values are given by  $q_t^+$  and  $\theta_1^+$ ,  $q_{t,ML}$  and  $\theta_{l,ML}$  indicate the mixed layer values and  $q_{sat,0}$  and  $\theta_{l,0}$  the surface values. The  $\theta_1$ -profile in the free troposphere is related to the surface value  $\theta_{l,ref}$ . The heights  $z_i$  and  $z_{cb}$  denote the inversion layer height and the cloud base height respectively.

budget equation for the conserved variables  $\psi$  is used:

$$z_{\rm i}\frac{\partial\psi_{\rm ML}}{\partial t} = F_{\psi,0} - F_{\psi,T} - \Delta S_{\psi}, \qquad (4.1)$$

which can be qualitatively understood as the change of the conserved variables in the mixed layer ( $\psi_{ML}$ ) by an inflow, outflow and a source/sink term. The derivation of the integrated budget equation can be found in section (B.2).

The values  $\psi_{\text{ML}}$  are governed by the turbulent flux at the surface  $F_{\psi,0}$ , at the top of the boundary layer  $F_{\psi,T}$  and  $\Delta S_{\psi}$  the total change of the source term between the surface and the top of the boundary layer. The latter can, for example, represent the effect of radiation.

The surface flux is obtained by using a bulk formula:

$$F_{\psi,0} = C_d U(\psi_0 - \psi_{\rm ML}), \tag{4.2}$$

with U the horizontal wind speed at the surface.

The flux at the top is proportional to the entrainment rate  $w_{\rm e}$  and the jump of  $\psi$  across the inversion:

$$F_{\psi,T} = -w_{\rm e}(\psi^+ - \psi_{\rm ML}),$$
 (4.3)

[Lilly, 1968]. The values  $\psi^+$  are just above the inversion layer, which is considered to have a very small thickness.

Substituting the surface and top fluxes into equation (4.1) gives:

$$z_{\rm i}\frac{\partial\psi_{\rm ML}}{\partial t} = C_d U(\psi_0 - \psi_{\rm ML}) + w_{\rm e}(\psi^+ - \psi_{\rm ML}) - \Delta S_{\psi}.$$
(4.4)

To complete the MLM, the boundary layer height  $z_i$  is needed. The inversion layer height grows because of entrainment, the mixing of warm and dry air into the boundary layer, but is counteracted by the subsidence, which is a mean vertical motion pushing on the boundary layer. The tendency of  $z_i$  is therefore given by:

$$\frac{\partial z_{\rm i}}{\partial t} = w_{\rm e} + \overline{w}.\tag{4.5}$$

Here  $\overline{w}$  represents the large-scale subsidence velocity.

#### 4.1 Boundary conditions

To solve the MLM equations, boundary conditions at height  $z_i^+$ , just above the inversion layer, are required. For the free troposphere the variation of the potential temperature is given by

$$\theta_{\rm l}(z) = \theta_{\rm l,ref} + \Gamma_{\theta} z, \qquad (4.6)$$

with lapse rate  $\Gamma_{\theta} = 6$  K km<sup>-1</sup> and  $\theta_{l,ref}$  the value of the potential temperature in the free troposphere extrapolated to the surface. The specific humidity in the free troposphere is taken constant such that no saturation occurs, usually  $0 \leq q_{t,ft} \leq 10$  g kg<sup>-1</sup>. The subsidence at the inversion layer height  $z_i$  is hard to measure, but can be estimated if the large-scale divergence of the horizontal wind is known as a function of height. Assuming the divergence does not depend on height, the subsidence reads:

$$\overline{w}(z_{i}) = -\int_{z=0}^{z_{i}} \left(\frac{\partial \overline{u}}{\partial x} + \frac{\partial \overline{v}}{\partial y}\right) dz = -\int_{z=0}^{z_{i}} D(z) dz = -Dz_{i},$$
(4.7)

with u and v the horizontal wind velocities [Stull, 1988, de Roode et al., 2012].

The drizzle source term  $\Delta S_{q_t}$  is set to zero. This is particularly applicable for a polluted environment in which clouds have a high droplet concentration and small drizzle fluxes. In the source term of the liquid water potential temperature, the radiative forcing is included, which has a cooling effect at the cloud top:

$$\Delta S_{\theta_{l}} = \frac{\Delta F_{rad}}{\rho_{air}c_{p}} = \Delta F.$$
(4.8)

The entrainment rate can be obtained from a ratio of a measure of buoyancy forcing to a measure of the inversion stability. For the entrainment rate different parameterisations have been developed from LES results and several are discussed by Stevens [2003]. De Roode et al. [2012] used the parameterisation by Nicholls and Turton in their MLM-studies, which can be written as:

$$w_{\rm e} = A \frac{w_*^3}{z_{\rm i} \Delta b},\tag{4.9}$$

with A the entrainment efficiency and

$$\Delta b \approx \frac{g}{\theta_0} \Delta \theta_{\rm v} \tag{4.10}$$

the buoyancy jump over the inversion, with g the acceleration due to gravity. The velocity scale  $w_*$  is a function of the vertical integral of the buoyancy flux:

$$w_* = \left(2.5 \frac{g}{\theta_0} \int_0^{z_i} \overline{w'\theta'_v} dz\right)^{\frac{1}{3}},\tag{4.11}$$

[Turton and Nicholls, 1987]. The Nicholls and Turton parameterisation is not trivial to apply in a two-layer model as it depends on the buoyancy flux throughout the whole mixed layer. In the two-layer model the cloud and sub-cloud layer are coupled through a transition layer, in which the buoyancy flux is not known. Throughout this research therefore another parameterisation is applied, used in earlier research from Dal Gesso et al. [2014b]:

$$w_e = \eta \frac{\Delta F}{\Delta \theta_1},\tag{4.12}$$

with efficiency factor  $\eta$  and  $\Delta \theta_l$  the liquid potential temperature inversion jump:  $\Delta \theta_l = \theta_l(z_i^+) - \theta_{l,ML}$ . The efficiency factor used by Dal Gesso et al. is  $\eta = 0.7$ .

### 4.2 Steady-state solutions

Steady-state solutions are easier to obtain than transient solutions since time as a variable is removed. In a steady-state solution, the entrainment rate balances the subsidence, as can easily be seen from equation (4.5):

$$w_{\rm e} = -\overline{w} = Dz_{\rm i}.\tag{4.13}$$

A steady-state solution for  $\theta_{l,ML}$  is found by combining the entrainment parameterisation of equation (4.12) and the heat equation (4.4):

$$\theta_{\rm l,ML} = \theta_{\rm l,0} - \frac{(1-\eta)\Delta F}{C_D U}.$$
(4.14)

An expression for  $q_{t,ML}$  is obtained from combining the budget equation (4.4) and equation (4.13):

$$q_{t,ML} = q_{t,0} + \frac{Dz_i(q_t^+ - q_{t,0})}{C_d U + Dz_i}.$$
(4.15)

The inversion layer height  $z_i$  follows from equation (4.13) and the entrainment parameterisation from equation (4.12):

$$z_{\rm i} = \frac{\eta \Delta F}{\Delta \theta_{\rm l} D}.\tag{4.16}$$

## 5 Two-layer model

The MLM assumes a well-mixed layer, with constant variables  $\psi$  that are the same in the sub-cloud and the cloud layer. However, observations show that the boundary layer does not remain well-mixed when it deepens [Nicholls, 1984, Albrecht, 1995, Betts, 1995]. The key process in the transition from stratocumulus to cumulus clouds is entrainment. Entrainment of free-tropospheric air into the stratocumulus-topped boundary layer (STBL) leads to deepening, which makes it increasingly difficult to sustain the mixing throughout the whole boundary layer [Nicholls and Leighton, 1985]. The eddies in the cloud layer become distinct from those in the sub-cloud layer and the STBL begins to separate into two layers: a cloud layer and a sub-cloud layer [Rogers and Koracin, 1992]. The BL is then said to be decoupled. The distinct eddies still mix the sub-cloud and the cloud layer separately, creating two mixed layers on top of each other. Cumulus clouds start to form at the top of the sub-cloud layer [Bretherton and Wyant, 1997, Park et al., 2004].



**Figure 5.1** – Schematic representation of the two-layer model. The two mixed layers, the cloud and sub-cloud layer are connected through the transition layer. The sub-cloud layer starts at the surface and ends at the sub-cloud layer height  $z_{\rm ML}$ . The cloud layer starts at the cloud base height  $z_{\rm cb}$  up to the inversion layer height  $z_{\rm i}$ . In the cloud layer the conserved variables are  $\theta_{\rm l,cld}$  and  $q_{\rm t,cld}$  and in the sub-cloud layer the conserved variables are  $\theta_{\rm l,ML}$ . The conserved variables in the transition layer are unknown and assumed to vary linaerly with height.

In the decoupled BL the conserved variables  $\psi$  are no longer the same in the cloud and sub-cloud layer, but are still constant with height in each individual layer due to vertical mixing within each layer. To describe such a decoupled BL a two-layered mixed layer model is used, that will be referred to as 'two-layer model'. A sketch of the profiles of conserved variables  $q_t$  and  $\theta_l$  is shown in figure 5.1. In this figure both the cloud layer and sub-cloud layer with different  $q_t$  and  $\theta_l$  are shown, where the cloud variables are indicated with  $q_{t,cld}$  and  $\theta_{l,cld}$  and the sub-cloud layer variables with  $q_{t,ML}$  and  $\theta_{l,ML}$ . The notation for the sub-cloud layer variables  $q_{t,ML}$  and  $\theta_{l,ML}$  might be somewhat confusing as it is the same notation as used in the MLM for the mixed-layer variables and it refers only to the sub-cloud layer as a mixed layer, while the cloud layer is also a mixed layer. This notation has been chosen nevertheless as it is the same as used in earlier work about decoupled boundary layers from Park et al. [2004].

The transition between the cloud layer and sub-cloud layer takes place in the transition layer. The exact profile inside this transition layer is unknown, but is here estimated as a linear interpolation between the cloud and sub-cloud variables.

To describe the boundary layer multiple variables are required. The variables  $q_t$ and  $\theta_l$  in both mixed layers are wanted, which determine the height of the subcloud layer and the cloud base. To determine the thickness of the cloud also the inversion layer height  $z_i$  is necessary. The inversion layer height is still determined by equation (4.5). To obtain  $q_t$  and  $\theta_l$  the integrated budget equations are used, for which the derivation can be found in section B.2. The budget equations for the cloud, transition and sub-cloud layer are:

$$\frac{\partial \psi_{\rm cld}}{\partial t} = \frac{w_{\rm e} \Delta \psi - \Delta S_{\rm cld} + F_{\psi, z_{\rm cb}}}{z_{\rm cld}}$$
(5.1)

$$\frac{\partial \psi_{\rm tr}}{\partial t} = \frac{-F_{\psi, z_{\rm cb}} + F_{\psi, z_{\rm ML}} - \Delta S_{\rm tr}}{z_{\rm cb} - z_{\rm ML}}.$$
(5.2)

$$\frac{\partial \psi_{\rm sub}}{\partial t} = \frac{-F_{\psi, z_{\rm ML}} - \Delta S_{\rm ml} + F_{\psi, 0}}{z_{\rm ML}},\tag{5.3}$$

with  $\Delta S$  the source term over the entire cloud or sub-cloud layer and cloud thickness  $z_{\rm cld} = z_{\rm i} - z_{\rm cb}$ . In the three equations (5.1), (5.2) and (5.3) there are five unknowns:  $\psi_{\rm cld}$ ,  $\psi_{\rm tr}$ ,  $\psi_{\rm ML}$ ,  $F_{\psi,z_{\rm ML}}$  and  $F_{\psi,z_{\rm cb}}$ . To get to a closure of the system,  $\psi_{\rm cld}$  and  $\psi_{\rm ML}$  are required to obey the relation found by Park et al. [2004]:

$$\psi_{\rm cld} = \psi_{\rm ML} + \alpha_{\psi} (\psi^+ - \psi_{\rm ML}), \qquad (5.4)$$

where  $\alpha_{\psi} \in (\alpha_{\theta}, \alpha_q)$  represents the so-called decoupling parameter. Following the paper of Park et al., Wood and Bretherton [2004] did an observational study and

found that  $\alpha_{\psi}$  could be well fit by:

$$\alpha_{\psi} = r_{\psi}(z_{\rm i} - z_{\rm ML}),\tag{5.5}$$

with  $z_{\rm ML}$  the height of the sub-cloud layer.

#### 5.1 Steady-state solution

The four equations (5.1), (5.2), (5.3) and (5.4) can be used to obtain the steady state of the boundary layer. As the changes over time are zero in steady state,  $\psi_{\rm tr}$  drops out of the equations leaving four equations and four unknowns:  $\psi_{\rm cld}$ ,  $\psi_{\rm ML}$ ,  $F_{\psi,z_{\rm ML}}$  and  $F_{\psi,z_{\rm cb}}$ .

No precipitation is taken into account and the radiative cooling takes place over a relatively thin layer and is therefore only considered in the cloud budget equation [Garrat, 1994]. With the fluxes at the top and surface known, the fluxes at  $z_{\rm cb}$  and  $z_{\rm ML}$  are wanted. From equation 5.2 it follows that they are related to each other by  $F_{\psi,z_{\rm ML}} = F_{\psi,z_{\rm cb}}$ . To express the fluxes  $F_{\psi,z_{\rm ML}}$  and  $F_{\psi,z_{\rm cb}}$  in known variables, equations 5.3 and 4.2 are combined to:

$$F_{\psi, z_{\rm ML}} = F_{\psi, z_{\rm cb}} = F_{\psi, 0} = C_d U \left( \psi_0 - \psi_{\rm ML} \right).$$
(5.6)

The only unknowns left are  $\psi_{\text{cld}}$  and  $\psi_{\text{ML}}$ . The first expression that can be used to solve  $\theta_{\text{l,ML}}$  is equation (5.6). A second expression for  $F_{\psi,z_{\text{ML}}}$  can be obtained from equation (5.1):

$$F_{\theta_{\rm l},z_{\rm cb}} = -w_{\rm e} \left(\theta_{\rm l}^+ - \theta_{\rm l,cld}\right) + \Delta F.$$
(5.7)

Combining these equations (5.6) and (5.7) and rewriting to solve  $\theta_{l,ML}$  results in:

$$\theta_{\rm l,ML} = \theta_{\rm l,0} + \frac{w_{\rm e} \left(\theta_{\rm l}^+ - \theta_{\rm l,cld}\right) - \Delta F}{C_d U}, \qquad (5.8)$$

which still contains two unknowns:  $\theta_{l,ML}$  and  $\theta_{l,cld}$ . To eliminate  $\theta_{l,cld}$ , the entrainment parameterisation from equation 4.12 can be used. The  $\theta_{l}$ -jump over the inversion layer is then substituted into equation (5.8) to obtain:

$$\theta_{\rm l,ML} = \theta_{\rm l,0} - \frac{(1-\eta)\,\Delta F}{C_d U}.\tag{5.9}$$

Now that  $\theta_{l,ML}$  is known,  $\theta_{l,cld}$  can be calculated using equation (5.4). The liquid water potential temperature in the sub-cloud layer does not depend on the rate of decoupling, but  $\theta_{l,cld}$  does. If the decoupling is very small:

$$\lim_{\alpha_{\theta} \to 0} \theta_{l,cld} = \theta_{l,ML}, \qquad (5.10)$$

since the two-layer model without decoupling reduces to the MLM. For very large decoupling:

$$\lim_{\alpha_{\theta} \to 1} \theta_{l,cld} = \theta_l^+, \tag{5.11}$$

where the cloud layer liquid potential temperature is pushed towards the free tropospheric  $\theta_1$ .

The remaining variables that need to be calculated are  $q_{t,ML}$  and  $q_{t,cld}$ . To solve  $q_{t,ML}$  the same strategy is used as for  $\theta_{l,ML}$ , with the only difference that there are no source terms for  $q_t$ . A first equation used to solve  $q_{t,ML}$  is (5.6). A second expression for  $F_{q_{t,z_{ch}}}$  can be found again from equation (5.1):

$$F_{q_{\rm t}, z_{\rm cb}} = -w_{\rm e} \left( q_t^+ - q_{\rm t, cld} \right).$$
 (5.12)

Combining equations (5.6) and (5.12) and rewriting leads to an expression for  $q_{t,ML}$ :

$$q_{\rm t,ML} = q_{\rm t,0} + \frac{w_{\rm e} \left(q_t^+ - q_{\rm t,cld}\right)}{C_d U},$$
 (5.13)

which still contains two unknowns:  $q_{t,ML}$  and  $q_{t,cld}$ . Here the entrainment parameterisation cannot be used to solve  $q_{t,ML}$ , as the equation involves the  $q_t$ -jump instead of the  $\theta_l$ -jump. A second equation containing both  $q_{t,ML}$  and  $q_{t,cld}$  was stated in equation (5.4). Combining equations (5.4) and (5.13) results in:

$$q_{\rm t,ML} = \frac{q_{\rm t,0} + \frac{w_{\rm e}}{C_d U} \left(1 - \alpha_q\right) q_t^+}{1 + \frac{w_{\rm e}}{C_d U} \left(1 - \alpha_q\right)} = \frac{C_d U q_{\rm t,0} + D z_{\rm i} \left(1 - r_q \left(z_{\rm i} - z_{\rm ML}\right)\right) q_t^+}{C_d U + D z_{\rm i} \left(1 - r_q \left(z_{\rm i} - z_{\rm ML}\right)\right)}, \quad (5.14)$$

where equations (4.12) and (5.5) are used to substitute  $w_{\rm e}$  and  $\alpha_q$ . Now that  $q_{\rm t,ML}$  is known, equation (5.4) can be used to obtain  $q_{\rm t,cld}$ . The total specific humidity in the sub-cloud and cloud layer depends on the rate of decoupling. If the decoupling is very small:

$$\lim_{\alpha_q \to 0} q_{t,ML} = q_{t,0} + \frac{Dz_i(q_t^+ - q_{t,0})}{C_d U + Dz_i},$$

$$\lim_{\alpha_q \to 0} q_{t,cld} = q_{t,ML},$$
(5.15)

giving the same solution as the steady state solution from the MLM in equation 4.15, since the two-layer model without decoupling reduces to the MLM. For very large decoupling

$$\lim_{\alpha_q \to 1} q_{t,ML} = q_{t,0},$$

$$\lim_{\alpha_q \to 1} q_{t,cld} = q_t^+,$$
(5.16)

where the humidity state of the sub-cloud layer is pushed towards the surface humidity  $q_{t,0}$  and the cloud layer is pushed towards the free tropospheric humidity. When observing equations (5.4) and (5.14) is becomes clear that to calculate  $q_{t,ML}$ ,  $q_{t,cld}$  and  $\theta_{l,cld}$  the inversion layer height  $z_i$  is needed and should be calculated. To obtain a relation for  $z_i$ , equations (5.4) and (5.14) are used:

$$r_{\theta}(z_{\rm i} - z_{\rm ML}) = 1 - \frac{\Delta \theta_{\rm l}}{\theta_{\rm l}^+ - \theta_{\rm l,ML}},\tag{5.17}$$

where  $\theta_{l,ML}$  depends on  $z_i$  and can be removed from the equation by substituting equation (5.9) into equation (5.17). Rearranging after this substitution gives:

$$[r_{\theta} (z_{\rm i} - z_{\rm ML}) - 1] \left[ \theta_{\rm l}^+ - \theta_{\rm l,0} + \frac{(1 - \eta) \Delta F}{C_d U} \right] + \Delta \theta_{\rm l} = 0.$$
 (5.18)

The  $\theta_{l}$ -jump depends on  $\theta_{l,cld}$  and therefore on  $z_{i}$ . To eliminate  $\Delta \theta_{l}$  from equation (5.18), the entrainment parameterisation from (4.12) is rewritten to obtain:

$$\Delta \theta_{\rm l} = \frac{\eta \Delta F}{w_{\rm e}} = \frac{\eta \Delta F}{Dz_{\rm i}},\tag{5.19}$$

where  $w_{\rm e} = -\overline{w} = Dz_{\rm i}$  according to the steady-state solution of equation (4.5) and the subsidence equation from equation (4.7). The substitution of equation (4.6) and (5.19) into equation (5.18) eliminates the last variables that depend on  $z_{\rm i}$ . This results in the equation:

$$z_{\rm i} \left[ r_{\theta} \left( z_{\rm i} - z_{\rm ML} \right) - 1 \right] \left[ \theta_{\rm l,ref} + \Gamma_{\theta} z_{\rm i} - \theta_{\rm l,0} + \frac{\left( 1 - \eta \right) \Delta F}{C_d U} \right] + \frac{\eta \Delta F}{D} = 0 \qquad (5.20)$$

that still involves one unknown: the sub-cloud layer height  $z_{\rm ML}$  where such a relative humidity (RH) is reached that condensation starts to occur. The RH-profile in the sub-cloud layer is determined by  $q_{\rm t,ML}$  and  $\theta_{\rm l,ML}$ , which cannot be calculated before calculating  $z_{\rm i}$ . In order to obtain an analytical solution, the approximation

$$\alpha_{\psi} = r_{\psi} \left( z_{\rm i} - z_{\rm ML} \right) \approx r_{\psi} z_{\rm i} \tag{5.21}$$

is used. This results in the polynomial

$$z_{i}^{3}r_{\theta}\Gamma_{\theta} + z_{i}^{2}\left\{r_{\theta}\left[\theta_{l,ref} - \theta_{l,0} + \frac{(1-\eta)\Delta F}{C_{d}U}\right] - \Gamma_{\theta}\right\}$$
  
+
$$z_{i}\left[-\theta_{l,ref} + \theta_{l,0} - \frac{(1-\eta)\Delta F}{C_{d}U}\right] + \frac{\eta\Delta F}{D} = 0,$$
(5.22)

that can be solved for  $z_i$ . The cloud base height is determined as the height in the cloud layer where condensation starts to occur. For this  $q_{\text{sat}}$  is calculated with equation (2.9) and  $\theta_{l,\text{cld}}$ . Then  $q_{t,\text{cld}}$  is compared with  $q_{\text{sat}}$  to determine the cloud base height.

#### 5.2 Transient Solutions

The four equations (5.1), (5.2), (5.3) and (5.4) with the five unknowns  $\psi_{\text{cld}}$ ,  $\psi_{\text{tr}}$ ,  $\psi_{\text{ML}}$ ,  $F_{\psi,z_{\text{ML}}}$  and  $F_{\psi,z_{\text{cb}}}$  are used to obtain the transient solutions of the two-layer model. To close the problem, a fifth equation is needed.



**Figure 5.2** – Schematic overview of the heat and moisture fluxes in a decoupled boundary layer. The numbers indicate the steps taken to obtain all the information needed to describe the evolution of the boundary layer. The explanation of all steps can be found in the text.

In figure 5.2 a schematic procedure of the steps in this section is shown. The steps in the text corresponding to the steps in the figure are indicated with (n), where n is the number of the step.

A fifth equation is obtained by relating the flux at the top of the sub-cloud layer to the flux at the surface by:

$$F_{\psi, z_{\rm ML}} = f_{\psi} F_{\psi, 0},$$
 (5.23)

with flux ratio  $f_{\psi}$  (1). From LES results and observations the ratio for the  $\theta_{\rm v}$ -flux is found to be approximately  $f_{\theta_{\rm v}} = -0.25$ . To obtain  $f_{\theta_{\rm l}}$  it can be used that for clear air

$$\overline{w'\theta'_{\rm v}} \approx A_d \overline{w'\theta'_{\rm l}} + B_d \overline{w'q'_{\rm t}},\tag{5.24}$$

with  $Ad \approx 1.01$  and  $B_d \approx 0.608\theta_{\rm ml}$  [de Roode et al., 2004]. It then follows that

$$f_{\theta_{l}} = f_{\theta_{v}} + \frac{B_{d}F_{q_{t},0}\left(f_{\theta_{v}} - f_{q_{t}}\right)}{A_{d}F_{\theta_{l},0}},$$
(5.25)

where from LES results of stratocumulus transition cases  $f_{q_t} = 0.9$  is suggested by van der Dussen et al. [2013]. Since the fluctuation of the humidity flux ratio over a diurnal cycle is a larger than the fluctuation of  $f_{\theta_l}$ ,  $f_{q_t}$  is only used to obtain  $f_{\theta_l}$ and the flux  $F_{q_t,z_{\rm ML}}$  is not fixed with this ratio as in equation (5.23).

A first attempt to close the problem did not succeed. The prescribed entrainment parameterisation from equation (4.12) led to a top flux for which  $F_{\theta_{1},T} + \Delta F > 0$ . The decoupling restriction requires the cloud layer to warm faster than the subcloud layer, resulting in an even larger  $F_{\theta_{1},z_{cb}}$ , as shown in figure 5.3. According to equation (5.23) the flux at the top of the sub-cloud layer  $F_{\theta_{1},z_{ML}}$  is however negative. The flux profile in the transition layer is determined by  $F_{\theta_{1},z_{ML}}$  and  $F_{\theta_{1},z_{cb}}$ . This flux profile then indicates that both cloud and sub-cloud layer are then warming, while the transition layer is rapidly cooling, which is very unrealistic.



**Figure 5.3** – A schematic overview of the heat flux in a decoupled boundary layer. The left profile indicates the first steps taken, where the flux profile on the right is completed. This flux profile was obtained in a first attempt to obtain a solution for the evolution of the boundary layer. It indicates the warming of the cloud and sub-cloud layer and the cooling of the transient layer, which is very unrealistic.

To avoid the transition layer from cooling while the rest of the boundary layer is warming, a linear flux profile has been chosen between the surface and the stratocumulus cloud base and the entrainment rate has not been fixed according to equation (4.12). The transition layer now follows the same tendency as the sub-cloud layer. A linear flux profile between  $z_{\rm ML}$  and  $z_{\rm i}$  would also have been a possibility, the transition layer would then follow the same tendency as the cloud layer. The first unknown to solve is  $\theta_{l,ML}$ . According to equation (5.3) the evolution of  $\theta_{l,ML}$  depends on the fluxes at the surface and at  $z_{ML}$ . The flux at the surface is known from equation (4.2) and the flux at  $z_{ML}$  is known from equation (5.23), so the tendency of  $\theta_{l,ML}$  is known and can be rewritten as:

$$\frac{\partial \theta_{\text{I,ML}}}{\partial t} = \frac{F_{\theta_{\text{I}},0} \left(1 - f_{\theta_{\text{I}}}\right)}{z_{\text{ML}}}.$$
(5.26)

To obtain the tendency of  $\theta_{l,cld}$  the fluxes at  $z_{cb}$  and the top are needed according to equation (5.1). Since a linear flux profile between the surface and the cloud base is assumed, the flux at  $z_{cb}$  can be written as:

$$F_{\theta_{l,z_{cb}}} = F_{\theta_{l},0} \left[ 1 + \frac{z_{cb}}{z_{ML}} \left( f_{\theta_{l}} - 1 \right) \right], \qquad (5.27)$$

(2). The top flux, however, depends on the entrainment rate according to:

$$F_{\psi,T} = -w_{\rm e} \left(\psi^+ - \psi_{\rm cld}\right).$$
 (5.28)

Therefore an entrainment rate should be found such that the cloud layer and subcloud layer are (de)coupled via equation (5.4) and such that the transition layer has the same tendency as the sub-cloud layer. To obey the decoupling of the cloud and sub-cloud layer the derivative of equation (5.4) with respect to time is used as a starting point:

$$\frac{\partial \theta_{l,cld}}{\partial t} = \alpha_{\theta} \frac{\partial \theta_{l}^{+}}{\partial t} + (1 - \alpha_{\theta}) \frac{\partial \theta_{l,ML}}{\partial t}.$$
(5.29)

The time derivative of  $\alpha_{\theta}$  is neglected. The time derivative of  $\alpha_{\theta}$  reads:  $\frac{\partial \alpha_{\theta}}{\partial t} = r_{\theta} \left( \frac{\partial z_{i}}{\partial t} - \frac{\partial z_{\text{ML}}}{\partial t} \right)$ , where the growth of  $z_{i}$  and the growth of  $z_{\text{ML}}$  oppose each other such that the tendency of  $\alpha_{\theta}$  is diminished. The tendency of the free tropospheric values is given by:

$$\frac{\partial \theta_{l}^{+}}{\partial t} = w_{e} \left(\frac{\partial \theta_{l}}{\partial z}\right)_{\text{free troposphere}} = w_{e} \Gamma_{\theta}.$$
(5.30)

Equations (5.1), (5.26) and (5.30) are substituted into equation (5.29) to obtain a relation for the entrainment rate  $w_e$ :

$$\frac{w_{\rm e}\Delta\theta_{\rm l} - \Delta F + F_{\theta_{\rm l}, z_{\rm cb}}}{z_{\rm cld}} = \alpha_{\theta} w_{\rm e} \Gamma_{\theta} + (1 - \alpha_{\theta}) \frac{F_{\theta_{\rm l}, 0} \left(1 - f_{\theta_{\rm l}}\right)}{z_{\rm ML}}.$$
 (5.31)

The entrainment rate now already obeys the decoupling between the cloud and sub-cloud layer. To make sure that the transition layer has the same tendency as the sub-cloud layer equation (5.27) is substituted in equation (5.31). Rearranging gives an expression for  $w_e$ :

$$w_{\rm e} = \frac{F_{\theta_{\rm l},0} \left\{ 1 + \frac{\left(f_{\theta_{\rm l}} - 1\right)}{z_{\rm ML}} \left[ z_{\rm i} \left(1 - \alpha_{\theta}\right) + \alpha_{\theta} z_{\rm cb} \right] \right\} - \Delta F}{\alpha_{\theta} \Gamma_{\theta} z_{\rm cld} - \Delta \theta_{\rm l}}.$$
(5.32)

Now that the entrainment rate is known, also the top flux  $F_{\theta_{l},T}$  from equation (5.28) can be calculated (3). Using this flux and  $F_{\theta_{l},z_{cb}}$  from equation (5.27) in equation (5.1) fixes the tendency of  $\theta_{l,cld}$  (4).

The profile of  $q_t$  is now still unknown. To obtain the tendency of  $q_{t,cld}$  the fluxes at the top and at the stratocumulus cloud base are required according to equation (5.1). The top flux  $F_{q_t,T}$  can be calculated according to (5.28) now that the entrainment rate is known (5). Since the fluxes are assumed linear from the surface to the stratocumulus cloud base, a relation for the flux  $F_{q_t,z_{cb}}$  is obtained:

$$F_{q_{\rm t}, z_{\rm cb}} = \frac{z_{\rm cb}}{z_{\rm ML}} \left( F_{q_{\rm t}, z_{\rm ML}} - F_{q_{\rm t}, 0} \right) + F_{q_{\rm t}, 0}, \tag{5.33}$$

which ensures that the tendency of the transient layer is equal to the tendency of the sub-cloud layer. This flux however depends on the flux  $F_{q_t,z_{\rm ML}}$ , which is still unknown. Since the flux ratio  $f_{q_t}$  is not fixed, as explained before,  $F_{q_t,z_{\rm ML}}$  cannot be calculated in the same way as  $F_{\theta_1,z_{\rm ML}}$ . The vertical profile of  $q_t$  should also obey the decoupling equation (5.4) and therefore this equation is used to obtain a second equation with the two unknowns  $F_{q_t,z_{\rm cb}}$  and  $F_{q_t,z_{\rm ML}}$ . The time derivative of equation (5.4) is taken and equations (5.1), (5.3) and (5.30) are substituted for the tendencies of  $q_{t,\rm cld}$ ,  $q_{t,\rm ML}$  and  $q_t^+$  respectively:

$$\frac{-F_{q_{t},T} + F_{q_{t},z_{\rm cb}}}{z_{\rm cld}} = \alpha_{q} w_{\rm e} \Gamma_{q} + (1 - \alpha_{q}) \frac{(-F_{q_{t},z_{\rm ML}} + F_{q_{t},0})}{z_{\rm ML}}.$$
 (5.34)

Combining the two equations (5.33) and (5.34) with the two unknowns gives an expression for the flux at the sub-cloud layer height:

$$F_{q_{t},z_{\rm ML}} = F_{q,0} + \frac{z_{\rm ML} \left( F_{q_{t},T} + \alpha_{q} z_{\rm cld} w_{\rm e} \Gamma_{q_{t}} - F_{q,0} \right)}{z_{\rm i} - \alpha_{q} z_{\rm cld}}, \qquad (5.35)$$

(6). Now that the fluxes at the surface and  $z_{\rm ML}$  are fixed, the tendency of  $q_{\rm t,ML}$  can be calculated according to equation (5.3). The flux at  $F_{q_{\rm t},z_{\rm cb}}$  is found according to equation (5.33), using the known  $F_{q_{\rm t},z_{\rm ML}}$  (7). With  $F_{q_{\rm t},z_{\rm cb}}$  and  $F_{q_{\rm t},T}$  the tendency of  $q_{\rm t,cld}$  is fixed according to equation (5.1).

Now that the vertical profiles of  $\theta_1$  and  $q_t$  are known and the inversion layer height is calculated according to equation (4.5), only the new  $z_{cb}$  and  $z_{ML}$  are needed. The new vertical profiles of  $\theta_{l}$  and  $q_{t}$  result in a new relative humidity profile. The height at which the RH reaches a critical point and condensation starts to occur will therefore be different with the new vertical profiles of  $\theta_1$  and  $q_t$ . This effect and subsidence prescribe the change of both  $z_{\rm ML}$  and  $z_{\rm cb}$ :

$$\frac{\partial z_{\rm ML}}{\partial t} = \frac{\partial z_{\rm ML} \left( {\rm RH} = {\rm RH}_{\rm crit} \right)}{\partial t} + \overline{w} \mid_{z_{\rm ML}}, \tag{5.36}$$

where a RH criterion  $RH_{crit}$  is set to slightly less than unity. The change of  $z_{cb}$  is given by:

$$\frac{\partial z_{\rm cb}}{\partial t} = \frac{\partial z_{\rm cb} \left( {\rm RH} = 1 \right)}{\partial t} + \overline{w} \mid_{z_{\rm cb}}, \tag{5.37}$$

where the cloud base is determined by the level at which the air is just saturated. The new heights of the layers are acquired. When considering these new heights and assuming that  $\theta_{l}$  and  $q_{t}$  in the cloud and sub-cloud layers do not change, the values in the transition layer should change. This can be seen by considering budget equation for the whole boundary layer, that consists of equations (5.1), (5.2) and (5.3):

$$z_{\rm cld}\frac{\partial\psi_{\rm cld}}{\partial t} + (z_{\rm cb} - z_{\rm ML})\frac{\partial\psi_{\rm tr}}{\partial t} + z_{\rm ML}\frac{\partial\psi_{\rm ML}}{\partial t} = -F_{\psi,T} + F_{\psi,0} - \Delta F.$$
(5.38)

Assuming that  $\psi_{\text{cld}}$  and  $\psi_{\text{sub}}$  do not change, but  $z_{\text{cb}}$  and  $z_{\text{ML}}$  do change,  $\psi_{\text{tr}}$  should change according to:

,

$$z_{\rm cld}\psi_{\rm cld} + (z_{\rm cb} - z_{\rm ML})\psi_{\rm tr} + z_{\rm ML}\psi_{\rm ML} = (z_{\rm cld} + dz_{\rm cld})\psi_{\rm cld} + (z_{\rm cb} + dz_{\rm cb} - z_{\rm ML} - dz_{\rm ML})(\psi_{\rm tr} + d\psi_{\rm tr}) + (z_{\rm ML} + dz_{\rm ML})\psi_{\rm ML}.$$
(5.39)

## 6 Set-up of the experiments

In this section the set-up of the experiments as well as the motivation to do these experiments is explained. The constants that are used for the experiments are displayed in table 6.1.

### 6.1 Transient solutions

The transient solutions are obtained as described in section 5.2. For the critical relative humidity  $RH_{crit} = 0.99$  has been chosen.

#### 6.1.1 Validation of the two-layer model

The two-layer model should accurately predict the development of the boundary layer over a period of time and should also be able to predict stratocumulus to cumulus transition as most of the uncertainties in cloud-climate feedback arise from the stratocumulus and stratocumulus to cumulus transition regimes [Williams and Webb, 2009].

To test the results from the two-layer model, the Atlantic Stratocumulus Transition EXperiment (ASTEX) is used as a reference. This field experiment was conducted in 1992 over the northeast Atlantic Ocean. In this experiment air traveling over sea was followed to study the stratocumulus to cumulus transition for a period of 40 hours. The initial profiles are taken from this case, as well as the time-varying boundary conditions such as the sea surface temperature and the large-scale divergence of horizontal winds.

Sandu and Stevens showed in an LES study that LES models can represent these cloud transition cases very well. The LES results obtained with DALES by Johan van der Dussen are therefor used to compare the results.

The radiative cooling has been set to the average net radiative cooling of ASTEX:  $\Delta F_{\rm rad} = 43 \text{ W/m}^2$ . All constants used from ASTEX are displayed in table 6.2.

Input parameter	Value	Input parameter	Value
$L_v$	$2.5008 \cdot 10^{6}$ J	$C_p$	$1004 \text{ J/(kg \cdot K)}$
U	10  m/s	g	$9.80665 \text{ m}/(s^2)$
$R_{ m d}$	287.06 J/(kg $\cdot$ K)	$p_0$	$1 \cdot 10^5$ Pa
$R_{ m v}$	$461.5 \ {\rm J}/({\rm kg} \cdot {\rm K})$	ρ	$1.1436 \ \rm kg/m^2$
$C_d$	0.001		

Table 6.1 – Input parameters for the experiments.

Input parameter	Value
$p_{\rm sfc}$	102900 Pa
$\Delta F_{\rm rad}$	$43 \mathrm{W/m^2}$
$\Gamma_{q_{\mathrm{t}}}$	$-2.8 \cdot 10^{-6} \text{ m}^{-1}$
$\Gamma_{ heta}$	$5.5 \cdot 10^{-3} \text{ K/m}$

Table 6.2 - Input parameters for the transient experiments.

#### 6.1.2 Subsidence experiment

A subsidence experiment is set up to determine the sensitivity of the development of the boundary layer, and in particular the LWP, to differences in subsidence. The motivation for this experiment is the uncertainty in the subsidence rate during the ASTEX transition [Bretherton and Pincus, 1995]. Bretherton and Pincus stated the hypothesis that the decreasing subsidence observed in ASTEX led to the break-up of the cloud layer.

However, in more recent research it is found that the decrease of subsidence actually leads to deepening of the cloud [de Roode and van der Dussen, 2010, Sandu and Stevens, 2011, van der Dussen, 2012, Bretherton et al., 2013].

The subsidence experiment in this thesis is conducted with three different divergences as a function of time, similar to the research done by van der Dussen [2012]. The different divergences used are introduced in section 7.3 and displayed in figure 7.7.

### 6.2 Steady-state solutions

This part of the research focuses on the steady-state solutions. The equilibrium solutions can only be physically representative if the adjustment time-scale of the boundary layer is much shorter than the time scale over which the forcings change [Zhang, 2009]. These steady state solutions are therefore very useful to research the feedback to climate changes. In this thesis these solutions will be used to study the feedback of clouds to an increase in SST. The steady-state solutions are obtained according to the method described in section 5.1.

To obtain the steady state solutions in a decoupled system, a decoupling parameter  $r_{\psi}$  must be used. Wood and Bretherton [2004] did an observational study to marine boundary layer depth and the degree of decoupling in different regions of the tropical and subtropical east Pacific. From these observations the median values of  $\alpha_{\theta}$  and  $\alpha_{q}$  have been found and are shown in table 6.3. The magnitude of the decoupling parameters can be estimated using the data of Wood and Bretherton from table 6.3 and the simplified relation:

$$\alpha_{\psi} \approx r_{\psi} z_i, \tag{6.1}$$

**Table 6.3** – Median values of  $\alpha_{\theta}$  and  $\alpha_{q}$  for five different regions [Wood and Bretherton, 2004].

Region	Longitude	Latitude	$lpha_{ heta}$	$lpha_q$	$\overline{z_i}$ [m]
a	$120^{\circ} - 130^{\circ} W$	$25^{\circ} - 35^{\circ}\mathrm{N}$	$0.15\pm0.08$	$0.18\pm0.06$	$1200\pm100$
b	$135^\circ - 150^\circ W$	$15^{\circ} - 25^{\circ}\mathrm{N}$	$0.30\pm0.10$	$0.32\pm0.08$	$1730\pm250$
с	$80^{\circ} - 90^{\circ} W$	$15^{\circ} - 25^{\circ}\mathrm{S}$	$0.11\pm0.07$	$0.13\pm0.06$	$1140\pm100$
d	$100^{\circ} - 110^{\circ}\mathrm{W}$	$5^{\circ} - 15^{\circ}\mathrm{S}$	$0.24\pm0.08$	$0.27\pm0.08$	$1560\pm200$
е	$90^{\circ} - 110^{\circ} \mathrm{W}$	$5^{\circ}\mathrm{S} - 5^{\circ}\mathrm{N}$	$0.29\pm0.08$	$0.33\pm0.07$	$1535\pm200$

that was introduced in equation (5.21) to allow for an analytical solution. Using this relation and the measurements of table 6.3,  $r_{\psi}$  is estimated in table 6.5. Based on these values  $r_q = 1.7 \cdot 10^{-4}$  and  $r_{\theta} = 0.89 r_q$  have been chosen.

Other parameters used for the steady-state experiments are given in table 6.4.

#### 6.2.1 Validation of the entrainment parameterisation

Since the Nicholls-Turton entrainment parameterisation is difficult to apply in a two-layer system, as explained in 4.1, the entrainment parameterisation of equation 4.12 is used. To test if it is valid to use this parameterisation, results from the two-layer model without decoupling are compared with results from de Roode et al., who used the Nicholls-Turton parameterisation.

#### 6.2.2 Steady-state experiments with the two-layer model

In the experiments of de Roode et al. the steady-state solutions of the boundary layer are obtained for different free tropospheric conditions. The ranges considered are 18 < LTS < 30 K and  $0 < q_{t,\text{ft}} < 10$  g/kg, which avoid condensation in the free troposphere.

The same experiments are done with the two-layer model to observe the effect of decoupling in the steady state of the boundary layer. The effect on the LWP is especially interesting, as the MLM tends to overestimate the LWP [Caldwell et al., 2012].

Table 6.4 – Input parameters for the steady-state experiments
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Input parameter	Value	Input parameter	Value
D	$5 \cdot 10^{-6} \text{ s}^{-1}$	$\Delta F_{rad}$	$40 \text{ W/m}^2$
SST	$289.5 { m K}$	$ heta_{ref}$	286 K
$p_{sfc}$	$101900 \ Pa$	$\Gamma_{ heta}$	$6 \cdot 10^{-3} \text{ K/m}$

Region	$r_{ heta}$	$r_q$	$\frac{r_{\theta}}{r_{q}}$
a	$1.3 \cdot 10^{-4} \pm 5.8 \cdot 10^{-6}$	$1.5 \cdot 10^{-4} \pm 4.2 \cdot 10^{-6}$	$0.87 \pm 4, 6 \cdot 10^{-2}$
b	$1.7 \cdot 10^{-4} \pm 8.2 \cdot 10^{-6}$	$1.8 \cdot 10^{-4} \pm 6.5 \cdot 10^{-6}$	$0.94 \pm 5.7 \cdot 10^{-2}$
с	$9.6 \cdot 10^{-5} \pm 5.4 \cdot 10^{-6}$	$1.1\cdot 10^{-4}\pm 4.5\cdot 10^{-6}$	$0.87 \pm 6.1 \cdot 10^{-2}$
d	$1.5 \cdot 10^{-4} \pm 6.4 \cdot 10^{-6}$	$1.7\cdot 10^{-4}\pm 6.5\cdot 10^{-6}$	$0.88 \pm 5.1 \cdot 10^{-2}$
е	$1.9\cdot 10^{-4}\pm 6.8\cdot 10^{-6}$	$2.1\cdot 10^{-4}\pm 5.8\cdot 10^{-6}$	$0.90 \pm 4.1 \cdot 10^{-2}$

**Table 6.5** – Deduced decoupling parameters  $r_{\theta}$  and  $r_q$  from equation 6.1 and table 6.3.

#### 6.2.3 Response LWP to perturbed SST

To discover the change in radiative effect of stratocumulus clouds in a warming climate, a steady state experiment is done in which the SST is perturbed by 1 K, similar to the experiment from de Roode et al. [2012]. Since the liquid water path (LWP) determines to the first order the albedo, the response of the LWP to a perturbed SST is examined.

### 7 Transient solutions with the two-layer model

The transient solutions are obtained according to the method described in section 5.2 and in the set-up described in section 6.1.

#### 7.1 Time evolution and comparison with LES results

In figures 7.1 and 7.2 the time evolutions based on the input from ASTEX can be seen for the two-layer model with decoupling parameters  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$  and for the case where there is no decoupling. Also the LES results obtained with DALES by van der Dussen et al. [2013] of the ASTEX case are plotted in the same figures to compare the model results with the LES results as explained in section 6.1. The vertical profiles of these results can be found in figure 7.3. The cloud and sub-cloud values of  $\theta_1$  and  $q_t$  have been estimated from the LES results.

In all model results the inversion layer height  $z_i$  grows in time. As an explanation, the entrainment causes a growth of  $z_i$ , while the subsidence  $\overline{w}$  pushes it down, but since  $w_e > \parallel \overline{w} \parallel$  there is a rapid growth in  $z_i$ . Both the MLM and the two-layer model overestimate  $z_i$  in the first 20 hours and after that underestimate  $z_i$ .

Due to a positive surface heat flux and the mixing of warm and dry air at the top of the cloud, the boundary layer warms. It can therefore be seen that  $\theta_{l,ML}$  and  $\theta_{l,cld}$  both increase with time. From the LES and the two-layer model results it can be seen that  $\theta_{l,cld}$  grows faster than  $\theta_{l,ML}$ . This is because the growing inversion layer height increases the amount of decoupling by equation (5.5). The increasing amount of decoupling pushes the cloud and sub-cloud layer further apart, causing the cloud layer to warm even more. In the case where ther is no decoupling,  $\theta_{l,ML}$ and  $\theta_{l,cld}$  are the same.

A positive surface humidity flux results in a moister sub-cloud layer as can be observed from the growth of  $q_{t,ML}$ . For the MLM the turbulent eddies are able to transport the moisture throughout the mixed layer. For the MLM  $q_{t,ML} = q_{t,cld}$  and therefore also  $q_{t,cld}$  grows in time. In the two-layer model the decoupling requires the cloud layer to be dryer than the sub-cloud layer. Dry and warm air is mixed into the cloud layer causing the drying of the cloud layer, which can be seen in the results of the two-layer model and the LES model. Even in a qualitative comparison of  $q_{t,cld}$  the MLM predictions are not correct, while the two-layer model gives similar results as the LES model.

The warming of the boundary layer leads to an increase in both  $z_{\rm cb}$  and  $z_{\rm ML}$ . Because of the drying of the cloud layer in the two-layer model,  $z_{\rm cb}$  becomes much higher there than in the MLM. For both  $z_{\rm ML}$  and  $z_{\rm cb}$  the two-layer model results are much closer to the LES results than the MLM results.

The predictions of the cloud thickness and LWP are much closer to the LES re-

sults when using the two-layer model instead of the MLM. The MLM predicts an increasing LWP in time, while the LES results show a decreasing LWP. The two-layer model is able to capture the same development as the LES model and also shows a decreasing LWP.

### 7.2 Effect of the decoupling rate on boundary layer evolution

In figures 7.4 and 7.5 time evolutions for different decoupling parameters are displayed. In figure 7.6 the vertical profiles of the same evolution are displayed at hours 20, 30 and 40.

For a larger decoupling,  $z_i$  grows faster. The entrainment rate obeys the decoupling equation (5.4) and therefore increases for a larger decoupling to warm and dry the cloud layer. As the entrainment rate determines the growth of the inversion layer,  $z_i$  grows faster for a larger decoupling.

From  $\theta_{l,cld}$  and  $q_{t,cld}$ , it can also be seen that for a larger rate of decoupling the cloud layer becomes dryer and warmer, as expected. The saturation point is therefore found at a higher level, explaining the increased  $z_{cb}$ .

Both  $z_i$  and  $z_{cb}$  increase for all decoupling parameter values, but for a larger decoupling  $z_{cb}$  grows faster than  $z_i$ . More decoupling therefore leads to smaller cloud thickness and a smaller LWP.

### 7.3 Effect of subsidence on the boundary layer evolution

To examine the influence of the subsidence on the transient solutions, three different large-scale divergences of horizontal winds have been used, as shown in figure 7.7. In figures 7.8 and 7.9 the time dependent solutions can be observed for the different divergences. In figure 7.10 the vertical profiles of  $\theta_1$  and  $q_t$  for hours 20, 30 and 40 are displayed.

The results show a faster growing  $z_i$  for smaller divergence. As an explanation, the entrainment causes the BL to grow, while the subsidence pushes it down. A smaller divergence leads to a smaller subsidence which results in a faster growing  $z_i$ .

A smaller divergence leads to a higher boundary layer, but also to more decoupling according to equation (5.5). The entrainment rate should obey the decoupling principle by the design of the two-layer model from section 5.2 and will increase to create a warming and drying of the cloud layer.

A different divergence has no influence on  $\theta_{l,ML}$  since its tendency depends on the surface flux according to equation 5.26 which is not influenced by the different divergence.

As a smaller divergence leads to a higher boundary layer, it also results in a larger



**Figure 7.1** – Time evolution of  $z_i$ ,  $z_{cb}$ ,  $z_{ML}$ ,  $z_{cld}$  and the LWP of the LES results and of the two-layer model with decoupling parameters  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$  and  $\text{RH}_{crit} = 0.99$ .



**Figure 7.2** – Time evolution of  $\theta_{l,ML}$ ,  $\theta_{l,cld}$ ,  $q_{t,ML}$ ,  $q_{t,cld}$  and  $w_e$  of the LES results and the two-layer model with decoupling parameters  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$  and  $\text{RH}_{crit} = 0.99$ .

decoupling according to equation (5.5). This larger decoupling results in a subcloud layer that is more moist. From equation (5.16) it could be seen that for larger decoupling the humidity state of the sub-cloud layer is pushed towards the surface humidity.

The increased entrainment rate for smaller subsidence leads to a dryer and warmer cloud, as warm and dry air from above the inversion is mixed into the cloud layer. Due to this warmer and dryer cloud layer, the cloud base height will also increase. For a smaller divergence both  $z_i$  and  $z_{cb}$  will get higher, but  $z_i$  grows more than  $z_{cb}$  leading to a thicker cloud. For smaller divergences the cloud thickness and therefore the LWP will be larger. This is accordance with earlier results by de Roode and van der Dussen [2010], Sandu and Stevens [2011], van der Dussen [2012], Bretherton et al. [2013].



**Figure 7.3** – The vertical profiles of  $q_t$  and  $\theta_l$  plotted for hours 20, 30 and 40 for decoupling parameters  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$  and  $\text{RH}_{\text{crit}} = 0.99$ . The line styles are the same as in figures 7.1 and 7.2.



**Figure 7.4** – Evolution of  $z_i$ ,  $z_{cb}$ ,  $z_{ML}$ ,  $z_{cld}$  and LWP for different decoupling parameters where  $r_{\theta} = 0.4r_q$  and RH<sub>crit</sub>= 0.99.



**Figure 7.5** – Evolution of  $\theta_{l,ML}$ ,  $\theta_{l,cld}$ ,  $q_{t,ML}$ ,  $q_{t,cld}$  and  $w_e$  for different decoupling parameters where  $r_{\theta} = 0.4r_q$  and  $\mathsf{RH}_{crit} = 0.99$ .



**Figure 7.6** – Vertical profiles of  $\theta_l$  and  $q_t$  for hours 20, 30 and 40 for different decoupling parameters. The line styles are the same as in figures 7.4 and 7.5.



**Figure 7.7** – Different divergences used, varying in time. The second divergence is the same as prescribed in the ASTEX case.



**Figure 7.8** – Time-dependent solutions of  $z_i$ ,  $z_{cb}$ ,  $z_{ML}$ ,  $z_{cld}$  and LWP for different divergences with  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$ .



**Figure 7.9** – Time-dependent solutions of  $\theta_{l,ML}$ ,  $\theta_{l,cld}$ ,  $q_{t,ML}$ ,  $q_{t,cld}$  and  $w_e$  for different divergences with  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$ .



**Figure 7.10** – Vertical profiles of  $\theta_l$  and  $q_t$  for three different divergences with  $r_q = 9 \cdot 10^{-4}$  and  $r_{\theta} = 0.4r_q$ . The linestyles are the same as in figures 7.8 and 7.9.

## 8 Steady-state solutions

The steady-state solutions are obtained with the method described in section 5.1 and the set-up of the experiments is described in section 6.2.

#### 8.1 Validation of the entrainment parameterisation

In figure 8.1 the steady-state solutions for the boundary layer for a range of free tropospheric conditions are showed, that are obtained by de Roode et al. [2012]. These are used as a reference to validate the use of the entrainment parameterisation given in equation (4.12).

In figure 8.2 the steady-state solutions in the same phase-space as the results from de Roode et al. are displayed. The efficiency factor used is  $\eta = 0.8$ . There are differences between the results obtained with different entrainment parameterisations. Due to a constant efficiency factor the free tropospheric humidity does not have any effect on the inversion layer height, while  $q_{t,ft}$  has an effect when using the Nicholls-Turton parameterisation. The same curvature as in the plots of de Roode et al. is therefore not found.

Apart from this small difference, the results obtained with the simple entrainment parameterisation are similar to those using a more advanced entrainment parameterisation such as the Nicholls-Turton parameterisation. Apparently the simple form used here is able to capture a similar behaviour.

To quantitatively approach the results of De Roode et al. as much as possible, different entrainment efficiencies have been used. In figure 8.3 and 8.4 the results for  $\eta = 1.0$  and  $\eta = 0.6$  are shown respectively. The efficiency factor of  $\eta = 0.7$ , used by Dal Gesso et al., gives results similar to figure 8.1 for higher LTS, while the high efficiency factor  $\eta = 1.0$  gives results more similar for lower LTS.

After comparing more results with different efficiency factors,  $\eta = 0.8$  is chosen to be an appropriate constant when using a constant  $\eta$ , since the results obtained then are close to the results obtained with the Nicholls-Turton entrainment parameterisation.

#### 8.2 Results with the two-layer model

The steady-state solutions of the boundary layer for a range of free tropospheric conditions are also obtained with the two-layer model to visualize the effect of the decoupling. The decoupling parameters used are  $r_q = 1.7 \cdot 10^{-4}$  and  $r_{\theta} = 0.89 r_q$  as explained in section 6.2. In figure 8.5 the steady state solutions with these decoupling parameters can be seen. When comparing these plots to the results of the MLM from figure 8.2, several differences are observed.

In the decoupled system  $\theta_{l,cld}$  is higher and  $q_{t,cld}$  lower, according to the design of



**Figure 8.1** – Steady-state solutions of the mixed layer model as a function of the LTS and  $q_{\rm t,ft}$  with Nicholls-Turton entrainment parameterisation. Figure copied from de Roode et al. [2012].

Single-layer model



Figure 8.2 – Steady-state solutions of the single-layer model as a function of the LTS and  $q_{\rm t,ft}, \eta = 0.8$ .

Single-layer model



Figure 8.3 – Steady-state solutions of the single-layer model as a function of the LTS and  $q_{\rm t,ft}, \eta = 1.0.$ 

Single-layer model



Figure 8.4 – Steady-state solutions of the single-layer model as a function of the LTS and  $q_{\rm t,ft}, \eta = 0.6$ .

the two-layer model. The warmer and dryer cloud results in a higher cloud base hight.

Due to the warmer and dryer cloud the temperature jump over the inversion layer has decreased, as can be seen from the higher entrainment rate  $w_{\rm e}$ . This entrainment leads to an increase in inversion layer height  $z_{\rm i}$ .

Despite the fact that  $z_i$  is higher than in the single-layer model, the LWP is smaller in the decoupled system, since  $z_{cb}$  increases more than  $z_i$ . As mentioned before, the MLM overpredicts the LWP [Caldwell et al., 2012]. This smaller LWP is more realistic when comparing these results to observations and LES results.

#### 8.2.1 Response LWP to perturbed SST

The effect of warming of the sea surface to the LWP is simulated by raising the SST as explained in section 6.2.3. In figure 8.6 the total response of the LWP can be seen for the MLM.

The LWP increases over the whole domain when raising the SST, indicating a cloud thickening for all free tropospheric conditions.

In figure 8.7 the total change of the LWP for perturbed SST is plotted for the two-layer model with decoupling parameters  $r_q = 1.7 \cdot 10^{-4}$  and  $r_{\theta} = 0.89 r_q$ , where the entrainment rate was allowed to respond to the change in SST.

Three areas can be distinguished. For very low values of  $q_{t,ft}$ , the response of the LWP is zero, indicated by the white area in the figure. This is because the LWP for this rate of decoupling is zero as can be seen from figure 8.5. The raise of SST does not change the absence of clouds and therefore the response of LWP to the raise in SST is zero.

For the lower part of the LTS values, a green area indicates the positive response of the LWP. The response to a sea surface warming is a cloud thickening, but the thickening is smaller than predicted by the MLM.

For the higher part of the LTS values, an orange area indicates the negatice response of the LWP. The two-layer model predicts a cloud thinning for these free tropospheric conditions, while the MLM predicts a cloud thickening for all free tropospheric conditions.

In figure 8.8 the response of the LWP to the change in SST is displayed for different decoupling parameters.

For small decoupling such as  $r_q = 1 \cdot 10^{-4}$  the response of the LWP is positive for most free tropospheric conditions. For large values of the LTS (LTS > 26 K) the response is negative.

Higher decoupling parameters  $(r_q \ge 2 \cdot 10^{-4})$  result in a larger part where the response of the LWP is zero. In these areas the steady-state solutions predict an LWP of zero. Changing the SST does not result in the formation of clouds and therefore the response of the LWP is also zero. Larger decoupling results in



**Figure 8.5** – Steady-state solutions of the two-layer model with  $r_q = 1.7 \cdot 10^{-4}$  and  $r_{\theta} = 0.89r_q$ .





**Figure 8.6** – Total response of the LWP in the single-layer model due to change in the SST. All responses of the LWP are positive.

**Figure 8.7** – Total response of the LWP in the two-layer model due to change in the SST. The decoupling parameters are  $r_q = 1.7 \cdot 10^{-4}$  and  $r_{\theta} = 0.89 r_q$ .

a larger domain of free tropospheric conditions where there are no clouds at all, mostly for small  $q_{t,ft}$ .

More decoupling  $(1 \cdot 10^{-4} \le r_q \le 4 \cdot 10^{-4})$  results in a larger free-tropospheric domain where the response of the LWP is negative. The only positive response found here is for a combination of low LTS and high  $q_{t,ft}$ .

Even more decoupling  $(r_q \ge 5 \cdot 10^{-4})$  results in large free-tropospheric domains without clouds. For high  $q_{t,ft}$  there are still clouds predicted. The response of the LWP is in this case negative.

Overall, the decoupled system predicts no clouds for small  $q_{t,ft}$ . For the other free tropospheric conditions the cloud response becomes smaller for higher decoupling rates resulting in an increasing area in the free-tropospheric phase-space where chloud thinning occurs instead of cloud thickening. Cloud thickening is only predicted for small decoupling parameters, low LTS and high  $q_{t,ft}$  but this thickening is less than predicted with the MLM.



**Figure 8.8** – Response of LWP to perturbed SST for different decoupling parameters with  $r_{\theta} = 0.89 r_q$ .

## 9 Conclusions

### 9.1 Transient solutions

A two-layer model that is more accurate than the MLM and able to predict the boundary layer evolution including the stratocumulus to cumulus transition is successfully developed in this research.

The two-layer model is able to predict a similar behaviour for the evolution of the boundary layer as the LES model for the ASTEX. Especially for the LWP, the results of the two-layer model are much more realistic than the results from the MLM. Moreover, the two-layer model can predict the cumulus cloud base similar to the results of the LES model, due to the condensation criterion  $RH_{crit}$  that is set in the sub-cloud layer.

The two-layer model developed in this research is able to predict the stratocumulus and stratocumulus to cumulus transition in a much better way than the MLM. The computational power needed for this model is small. The two-layer model is therefore a good tool to examine the effect of different perturbations in different cloud controlling factors.

The sensitivity of the development of the boundary layer to a different subsidence has been done by prescribing different divergences.

A smaller divergence led to a deeper BL and a larger LWP. In all two-layer model results for different divergences the LWP still decreases over time, indicating a cloud break-up. This was also found in the LES results from ASTEX.

Even though the entrainment rate is larger for a smaller subsidence, it results in a slower break-up of the stratocumulus cloud deck. The extra warming and drying of the cloud layer results in a higher cloud base, but it also results in a higher  $z_i$ . The increase in  $z_i$  is larger than the increase in  $z_{cb}$  due to a smaller subsidence rate, leading to a slower break-up. This confirms the earlier results from de Roode and van der Dussen [2010], Sandu and Stevens [2011], van der Dussen [2012], Bretherton et al. [2013].

### 9.2 Steady-state solutions

A strong dependency of the response of the LWP on the free tropospheric conditions was detected in the steady state solutions. This is in correspondence with the results from Roode et al. [2012]. The MLM predicted a cloud thickening and therefore a negative cloud radiative feedback for all free tropospheric conditions. A larger thickening was found for smaller LTS and higher  $q_{t,ft}$ .

The two-layer model predicts cloud thickening or thinning depending on the free

tropospheric conditions and decoupling rates. For small  $q_{t,ft}$  the two-layer model does not predict stratocumulus at all. The two-layer model predicts a thickening for high  $q_{t,ft}$  and low LTS. This thickening is smaller than in the prediction of the MLM. For high LTS, the two-layer model predicts a cloud thinning. A larger decoupling rate results in a larger area where no stratocumulus clouds are predicted, a larger area where cloud thinning is predicted, and a smaller area where cloud thickening is predicted.

The two-layer model mostly predicts a cloud thinning for larger decoupling rates, resulting a positive cloud radiative feedback. This is in accordance with LES results of the cloud radiative feedback for a stratocumulus and a decoupled stratocumulus case.

## 10 Recommendations

The two-layer model developed in this research is able to predict the stratocumulus and stratocumulus to cumulus transition in a much better way than the MLM. The results of the two-layer model and the LES model give remarkably similar results for the ASTEX case. Some effects are not taken into account however.

The radiative cooling in the two-layer model is taken to be the average net radiation from ASTEX. As an improvement in the transient predictions of the two-layer model, the diurnal variation in the radiation could be implemented in the model.

Another process not taken into account is precipitation. As mentioned before, this means that the results are particularly applicable to a polluted environment in which clouds have a high droplet concentration and small drizzle fluxes. An MLM study of the effect of droplet concentration on the cloud thickness was done by Wood [2007].

For the ASTEX case however, van der Dussen found that the precipitation contribution is only significant in the first part of the transition.

To close the transient solutions of the two-layer model, a linear flux profile between the surface and the stratocumulus cloud base height was assumed. As explained in section 5.2, a linear flux profile between the sub-cloud layer height and the inversion layer height would also have been an option. Due to the decoupling, the cloud layer warms faster than the sub-cloud layer. The transient layer might therefore be warming with a tendency closer to the cloud layer than the sub-cloud layer and a linear flux profile between the sub-cloud layer height and the inversion layer height would perhaps be more realistic.

The radiative cooling in this research is taken constant. Dal Gesso et al. use a more realistic  $\Delta F$  that is linearly dependent on  $q_t^+$  in their steady-state experiments, based on earlier sensitivity studies of Fouquart [1988] and Morcrette [1991]. As one of the ranges in the phase-space considers  $q_{t,ft}$ , the effect of a linearly dependent  $\Delta F$  instead of a constant  $\Delta F$  could easily be seen.

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# A List of Symbols

Abbreviation	Meaning
A	Scaling factor
$A_{d,w}$	Dry and wet coefficient
$B_{d,w}$	Dry and wet coefficient
$C_d$	Drag coefficient
D	Divergence of wind velocity
$F_{\psi}$	Flux of conserved variable $\psi$
$L_v$	Specific latent heat
LES	Large eddy simulation
LTS	Lower tropospheric stability
LWP	Liquid water path
MLM	Mixed layer model
R	Ideal gas constant
Ri	Richardson number
$S_{\psi}$	Source term for conserved variable $\psi$
SST	Sea surface temperature
T	Temperature
U	Horizontal wind velocity
$c_p$	Specific heat capacity
$e_s$	Saturation vapor pressure
$f_\psi$	Flux ratio
g	Gravity constant
m	Mass
p	Pressure
$p_0$	Reference pressure
$q_l$	Liquid specific humidity
$q_{\mathrm{sat}}$	Saturation specific humidity
$q_t$	Total specific humidity
$r_k$	Mixing ratio
$r_\psi$	Decoupling parameter for conserved variable
$s_l$	Liquid static energy
w	Velocity in vertical direction
$\overline{w}$	Large-scale subsidence velocity
$w_{ m e}$	Entrainment rate
$z_{ m cb}$	Cloud base height
$z_{ m cld}$	Cloud thickness
$z_{\mathrm{i}}$	Height of inversion layer
$z_{ m ML}$	Height of sub-cloud layer

 $\psi$ 

Abbreviation	Meaning
$\Gamma_{\psi}$	Lapse rate in free troposphere
Θ	Virtual potential temperature flux
П	Exner function
$lpha_\psi$	Decoupling parameter for conserved variable $\psi$
$\epsilon$	Emmissivity
$\eta$	Efficiency factor in entrainment parameterisation
$\theta$	Potential temperature
$ heta_l$	Liquid potential temperature
$ heta_v$	Virtual potential temperature
$\phi$	Cloud controlling factor
$\psi$	Thermodynamic property, $q_{\rm t}$ or $\theta_{\rm l}$
$\psi^+$	$\psi$ just above the inversion
ρ	Density
$\sigma$	Stefan-Boltzmann constant

## **B** Derivations of equations

#### **B.1** Potential Temperature

An air parcel at different heights will experience different pressures and also different temperatures. To be able to compare air parcels, the potential temperature has been introduced. This potential temperature is a temperature that is not influenced if a parcel of air moves adiabatically. The equation for potential temperature can be deduced from the first law of thermodynamics;

$$du = dq - dw = dq - pdv. (B.1)$$

With the use of the equation for the enthalpy

$$dh = du + pdv + vdp, \tag{B.2}$$

and using the definition for the isobaric specific heat

$$c_p \equiv \left(\frac{\partial h}{\partial T}\right)_p,\tag{B.3}$$

the first law can be rewritten as

$$dq = c_p dT - v dp. \tag{B.4}$$

When considering an air parcel that undergoes an adiabatic process, no heat exchange occurs, dq = 0. Using the ideal gas law, equation B.4 becomes

$$\frac{c_p}{T}dT = \frac{R_d}{p}dp,\tag{B.5}$$

which can be integrated from a pressure p and temperature T to a reference pressure  $p_0$  and reference temperature  $\theta$ :

$$\int_{T}^{\theta} \frac{c_p}{T} dT = \int_{p}^{p_0} \frac{R_{\rm d}}{p} dp.$$
(B.6)

From this the potential temperature  $\theta$  can be found:

$$\theta = T\left(\frac{p_0}{p}\right)^{\frac{R_d}{c_p}}.$$
(B.7)

Here the potential temperature and the actual temperature are related by the so called exner function  $\Pi$ 

$$\Pi = \left(\frac{p}{p_0}\right)^{\frac{\kappa_d}{c_p}} = \frac{T}{\theta}.$$
(B.8)

#### **B.2** Mixed Layer Model budget equation

For any conserved variable  $\psi$  the conservation equation in differential form can be written as

$$\frac{D\psi}{Dt} = \frac{\partial\psi}{\partial t} + u_i \frac{\partial\psi}{\partial x_i} = \frac{\partial S}{\partial x_i},\tag{B.9}$$

where S represents a flux source. Using the Reynolds averaging method and assuming small mean horizontal gradients, it can be derived that

$$\frac{\partial \overline{\psi}}{\partial t} = -\overline{w} \frac{\partial \overline{\psi}}{\partial t} - \frac{\partial \overline{w'\psi'}}{\partial z} - \frac{\partial \overline{S}}{\partial z}.$$
(B.10)

In the boundary layer  $\overline{\psi} = \psi_{ML}$  is constant with height up to the base of the inversion layer. Vertical integration of equation (B.10) then gives

$$z_i \frac{\partial \psi_{ML}}{\partial t} = -\overline{w'\psi'}|_{z_i} + \overline{w'\psi'}|_0 - \overline{S_\psi}|_{z_i} + \overline{S_\psi}|_0, \qquad (B.11)$$

where the subscript  $z_i$  refers to the values at the top of the mixed layer and the subscript 0 refers to the surface values. The conserved variables  $\psi$  are governed by the surface flux  $F_{\psi,0} = \overline{w'\psi'}|_0$ , the flux at the top of the inversion layer  $F_{\psi,T} = \overline{w'\psi'}|_{z_i}$  and the total change between the source term at the surface and at the top of the boundary layer  $\Delta S_{\psi} = \overline{S_{\psi}}|_0 - \overline{S_{\psi}}|_{z_i}$ . Equation (B.11) can then be rewritten as

$$z_i \frac{\partial \psi_{ML}}{\partial t} = F_{\psi,0} - F_{\psi,T} - \Delta S_{\psi}.$$
 (B.12)

The surface flux  $\overline{w'\psi'}|_0$  can be obtained by

$$\overline{w'\psi'}|_0 = C_d U(\psi_0 - \psi_{ML}), \qquad (B.13)$$

with drag coefficient  $C_d$  and U the horizontal wind speed. The flux at the top of the inversion layer is taken as

$$\overline{w'\psi'}|_{z_i} = -w_e(\psi(z_i^+) - \psi_{ML}), \qquad (B.14)$$

with entrainment  $w_e$  and the jump of conserved variable  $\psi$  across the inversion [Lilly, 1968]. The values at  $z_i^+$  are just above the inversion layer, which is considered to have a very small thickness. The conservation equation can then be rewritten as

$$z_i \frac{\partial \psi_{ML}}{\partial t} = C_d U(\psi_0 - \psi_{ML}) + w_e(\psi(z_i^+) - \psi_{ML}) - \Delta S_{\psi}.$$
 (B.15)